Chromatography

The separation process involving the interaction of one or more solutes and two phases.

Mobile phase

A gas or liquid that passes through a 'column'

Stationary phase

A solid or liquid which does not move.

Chromatography

Chromatography - "color" and "to write"

Originally described by Tswett - 1906

He devised a method to separate plant pigments using a tube filled with CaCO₃.

After adding a plant extract, he was able to produce several colored bands by washing the extract through the column with an organic solvent.

The separation process

Sample components are carried by a mobile phase through a bed of stationary phase.

Individual species are retarded by the stationary phase based on various interactions such as:

Surface adsorption Relative solubility Charge

Types of separation

Frontal analysis

Continuously add your sample to the start of the column.

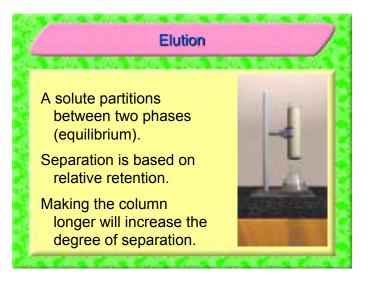
Monitor components as they evolve.

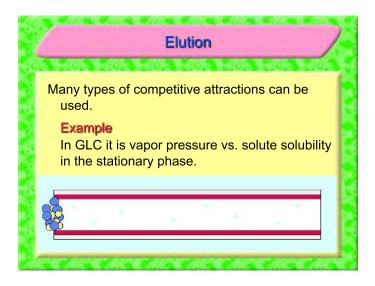
Gives a general measure of how things are retained.

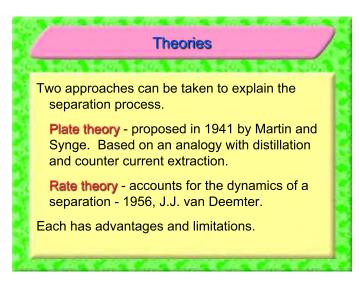
Example - charcoal filtration

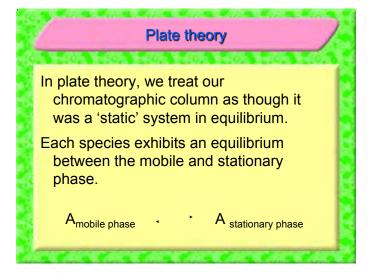
sample volume Approach can be used to evaluate relative retention. Not useful as a method of separation.

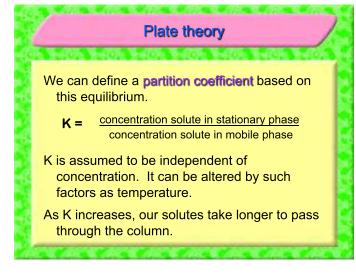
Materials move down a column by being displaced by a more highly retained solute. Example - ion exchange / water softeners You can't achieve complete resolution. Making the column longer has no effect

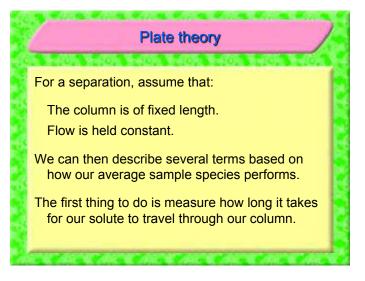












Retention time and volume

Retention volume, V_R - volume of mobile phase required to elute a solute to a maximum from a column.

Retention time, t_R, time required to reach the same maximum at constant flow.

$$V_R$$
 or t_R .

where $V_R = t_R x$ flowrate

Plate theory

The average linear rate for the solute is:

$$v = L / t_R$$

where L is the column length.

And for the mobile phase it is:

$$u = L/t_R$$

This is simply the time required for a noninteracting substance to pass through the column.

Plate theory

$$v = u \times f$$

f is the fraction of time that the solute spends in the mobile phase.

Since both the mobile and stationary phases have known volumes (V_M, V_S), we can now determine K - our partition coefficient.

Plate theory

$$V = u \frac{C_{M}V_{M}}{C_{M}V_{M} + C_{M}V_{S}}$$

$$= u \left(\frac{1}{1 + \frac{C_{S}V_{S}}{C_{M}V_{M}}} \right)$$

$$= u \left(\begin{array}{c} 1 \\ 1 + \frac{KV_S}{V_M} \end{array} \right)$$

Plate theory

$$v = u \left(\begin{array}{c} 1 \\ 1 + K V_S / V_M \end{array} \right)$$

This shows the factors required to have a component elute and how two materials can be separated.

Each material has its own K.
As K increases, elution takes longer.

Other terms affect the overall separation.

Plate theory

Raising

V_S General increase in retention
 V_M General decrease in retention
 u Increases speed of separation.

V_S and V_M can be altered by changing column diameter and length for a specific column packing.

u can be altered by changing the flowrate.

All terms can be found by knowing how the column was prepared.

Capacity factor

We'd like to be able to simply inject a sample and obtain the information we need from the results.

Capacity factor

$$K' = K V_S / V_M$$
 (constant for our column conditions)

so
$$v = u (1/(1 + k'))$$

We can now expand the equation.

Capacity factor

$$\frac{L}{t_R} = \frac{L}{t_M} \times \frac{1}{1+k}$$

$$k' = \frac{t_R - t_M}{t_M}$$

We now have a simple method to determine k values based on elution times.

Selectivity factor - a

Remember, the goal of chromatography is to 'separate' two or more species.

Since each species has its own k value, we need a way to tell if two species can be separated.

Selectivity factor

$$K_b > K_a, \alpha \ge 1$$
 $\alpha = \frac{K_B}{K_A}$

Selectivity factor

We can also use:

$$\alpha = \frac{\mathbf{k'_a}}{\mathbf{k'_b}} = \frac{\mathbf{t_{RB}} - \mathbf{t_M}}{\mathbf{t_{RA}} - \mathbf{t_M}}$$

You can either:

Determine $\boldsymbol{\alpha}$ based on the retention times for you solutes or

Estimate if your species are separable based on $\boldsymbol{\alpha}.$

Mechanism of component separation

Mobile phase volume is proportional to column length so retention is also increased for longer columns.

However, as peaks travel through the column, they broaden. Width increases with the square root of column length.

You can't just make a column longer to obtain a 'better' separation.

Theoretical plates - N

- In solvent extraction, a plate is represented by each equilibrium (extraction) we conduct.
- In a chromatographic column, we can't see these plates so they are theoretical.
- We can estimate the number of theoretical plates in our column based on peak retention times and widths.
- Both factors are important in determining if a separation will work.

The number of plates can be determined from the retention time and peak width. It doesn't matter what units are used as long as they are the same.

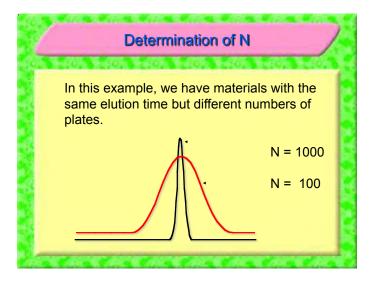
Determination of N

The number of plates is then calculated as:

$$N = 16 \left(\begin{array}{c} t_R \\ W \end{array} \right)^2$$

This approach is taken because peaks evolve as Gaussian-like shapes and can be treated statistically.

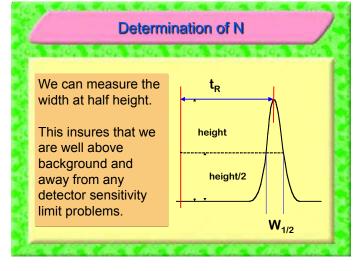
In essence, we are taking $\pm 2 \sigma$.



Determination of N

It is often difficult to accurately measure peak width.

- → The peak may co-elute with another.
- Low detector sensitivity can result in you finding the start or end at the wrong place.
- → We can take an alternate approach.



Determination of N

Since the peak is Gaussian in nature, we end up with the following modified formula.

$$N = 5.54 \left(\frac{t_R}{W_{1/2}} \right)^2$$

For a fixed length column, we can calculate an additional term - h (or HETP)

h = height equivalent of a theoretical plate = column length / N

Resolution

Knowing how well a column can retain a component is nice but we need to deal with multiple eluents or why bother.

Resolution, R_s

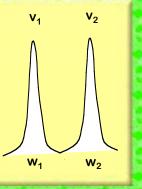
A measure of how completely two neighboring peaks are separated from each other.

Resolution

$$R_s = \frac{V_2 - V_1}{(W_2 + W_1)/2}$$

since w = $4 \text{ v / N}^{1/2}$

Note: times or any representative unit can be used in place of v and w terms.



Resolution

Since

$$v = V_m (1 - k)$$

resolution in terms of k is:

$$R_{s} = \frac{N}{2} \frac{k_{2} - k_{1}}{2 + k_{2} + k_{1}}$$

Remember that the relative volatility, α , is

$$\alpha = k_2 / k_1$$

Resolution

$$R_s = \frac{N}{2} \frac{\alpha - 1}{\alpha + 1 + 2/k_1}$$

Finally, if we define k as $(k_1+k_2)/2$ - average k

$$R_s = \frac{N}{4} \quad \begin{array}{ccc} \alpha - 1 & k \\ \alpha + 1 & 1 + k \end{array}$$

This version of the resolution equation will be most useful with LC.

Approximate resolution equations

The exact resolution equation is:

$$R_s = \frac{N}{4} \ln(1 + \frac{k_2 - k_1}{1 + k_1})$$

 $k_2 = k_1$, when $k_2 - k_1$ $1 + k_1$ is small compared to 1. and $\ln (1 + x) = x$

For a small x,
$$R_s = \frac{N}{4} {k_2 - k_1 \choose 1 + k_1}$$

Approximate resolution equations

Since $\alpha = k_2/k_1$, we get

$$R_s = \frac{N}{4} (\alpha - 1) \frac{k_1}{1 + k_1}$$
 Knox equation

Similarly, if we start with

$$R_s = -\frac{N}{4} \ln \left(1 - \frac{k_2 - k_1}{1 + k_1}\right)$$

This will lead to the Purnell Equation

$$R_s = \frac{N}{4} \frac{\alpha - 1}{\alpha} \frac{k_2}{1 + k_2}$$

Approximate resolution equations

Each version of the equation will yield R_s values that deviate from the exact solution.

Knox - R_s values will be higher

Purnell - R_s values will be lower

(a more conservative estimate)

If we assume that the peaks are Gaussian, we

an us: R_s = 1.18 W_{1/22} + W_{1/21}

A 'working' form of the resolution equation.

Example

Determine the k, N and HETP for toluene in the following analysis

> $W_{1/2}$, min Solute t_R, min 1.5 air 1.05 7.45 benzene 1.45

10.6

Column length = 10 meters Flow rate = 30 ml/min

isothermal conditions

toluene

Example

k

$$t_R / t_M = 1 + k$$

 $k = t_R / t_M - 1$

= 10.6 / 1.50 - 1

= 6.07

Example

N = 5.54 (
$$t_R / W_{1/2}$$
)²

$$= 5.54 (10.6 / 1.45)^{2}$$

= 296

HETP

Example

Finally, calculate the resolution between the benzene and toluene peaks.

$$R_{s} = 1.18 \frac{(t_{toluene} - t_{benzene})}{(W_{1/2 toluene} + W_{1/2 benzene})}$$

= 1.18 (10.6 - 7.45) / (1.05 + 1.45)

= 1.48 (quantitative separation)

Rate theory of chromatography

Plate theory assumes that a column is mathematically equivalent to a plate column.

An equilibrium is established for the solute between the mobile and stationary phases one each plate.

It is a useful theory and can predict many aspects of chromatographic performance.

Rate theory of chromatography

Plate theory neglects the concepts of solute diffusion and flow paths.

Rate theory accounts for these and can be used to predict the effect on column performance factors such as:

> phase properties solute diffusivitivites partition coefficients phase velocity

phase thickness support size support porosity flow rates

Rate theory of chromatography

A partial differential equation set up by van Deemter for a linear isotherm resulted in an effluent concentration function.

It is based on a Gaussian distribution similar to that of plate theory.

He was attempting to account for the dynamics of the separation process.

van Deemter equation

H =
$$2 \lambda d_p + \frac{2 \gamma D_g}{u} + \frac{8 k d_f^2}{\pi^2 (1+k)^2 D_l} u$$

- factor characteristic of packing

- particle diameter

- factor for irregularity of interparticle spaces - diffusion coefficient of compound in gas

D_g

- diffusion coefficient of compound in liquid

k

- capacity ratio

- liquid phase effective film thickness

df Н

- linear gas velocity

- height of a theoretical plate

van Deempter equation

The equation consists of three basic terms.

 $2 \lambda d_{\rm p}$

Packing related term

 $2 \gamma D_{\alpha}$

Gas (mobile phase) term

π² (1+k)² D₁ u Liquid (stationary phase) term

van Deemter equation

We commonly group the various constants into single terms and reduce the equation to:

$$H = A + B/u + Cu$$

multipath or eddy diffusion

molecular diffusion

resistance to mass transfer

Note that A, B and C are constants but the effect of B and C is dependent of the velocity of the mobile phase.

van Deemter equation

The goal is to find H_{min} for optimum column performance.

$$H = A + B/u + Cu$$

B/u

H

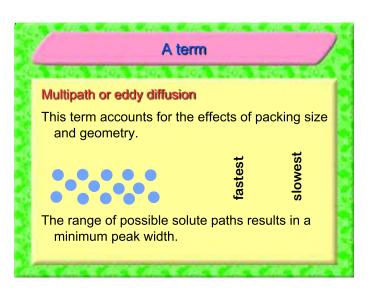
Cu

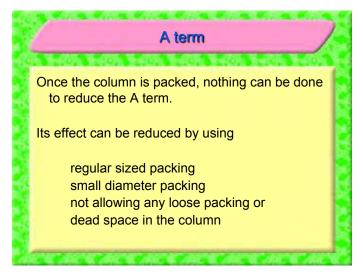


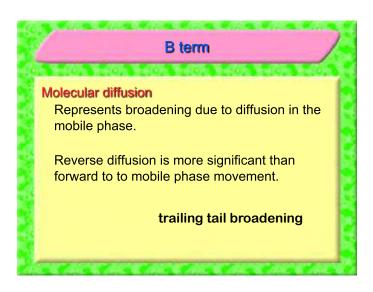
For a packed

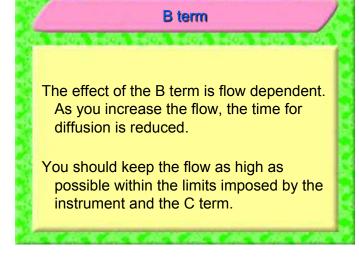
GC column

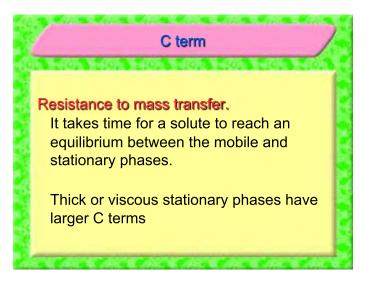
You don't need to calculate H for each column/eluent combination to be able to use this relationship. An understanding of the effects of each term will help you design/select appropriate columns and optimum flows.



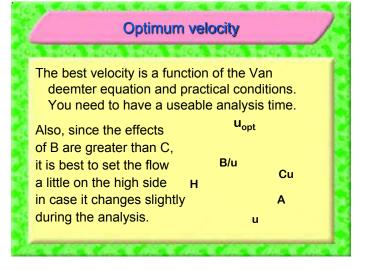


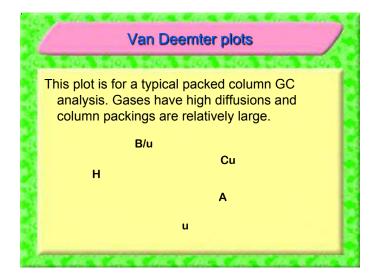


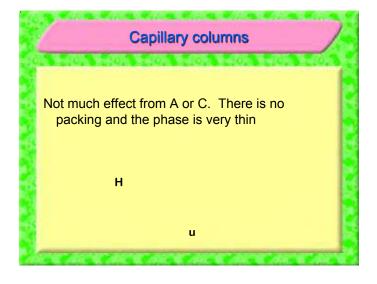




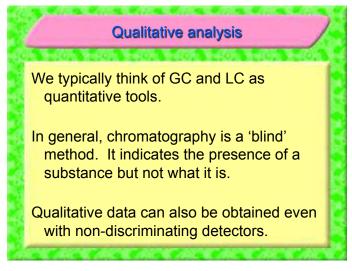
C term You can minimize the effect of the C term by: Using "thin" coatings of the stationary phase on a solid support. Use less viscous phases. Keep the flow as low as possible - limited by the effect of the B term.







At first, LC relied on irregular packing. Now the packings are pretty good so the A term is very low. The B and C terms are low because liquids H diffuse much more current slowly than gases



Qualitative analysis

Retention data - can be used for some qualitative work. The t_R is characteristic of a substance, compared to a standard. To be useful, some problems must be addressed.

- Reproducibility of absolute retention data depends on several experimental conditions.
- Is t_R, v_R, v'_R or t'_R best to use?

Retention time

Retention time - t_R - time elapsed from point of injection to maximum of peak.

Adjusted t_R - t'_R - time from maximum of unretained peak to maximum of eluent.

Hold up time - t_M - time required for mobile phase to traverse the column.

Retention volumes

If the flowrate (F_c) is constant and known then:

Retention volume =
$$V_R$$
 = t_R F_c

Adjusted
$$V_R$$
 = V'_R = t'_R F_c

Hold up volume =
$$V_m$$
 = $t_M F_c$

Retention relationships

Retention volume or time may be used for identification.

For a homologous series, V_R can be accurately determined by:

$$\ln V'_n = a + bn$$

where V'_n = adjusted retention volume

n = carbon number

a, b = fit parameters

and $V'_n = V_n - V_m$

Retention relationships

To determine an unknown carbon number:

$$x = n_1 + (n_2-n_1) \frac{InV_x - InV_{n1}}{InV_{n2} - InV_{n1}}$$

$$n_2 > x > n_1$$

This can only be used for straight chain compounds and the unknown must fall between n_1 and n_2 .

Absolute retention index

For non-paraffins, we can simply calculate an index value like it was a paraffin. The value does not need to be a whole number.

$$I_p = n_1 + \frac{InV_x - InV_{n1}}{InV_{n2} - InV_{n1}}$$

$$n_2 > x > n_1$$

n₂ and n₁ are reference paraffins.

Kovat's retention index

A modification of the absolute index where:

$$I_K = 100 I_P = 100n_1 + 100 \frac{InV_x - InV_{n1}}{InV_{n2} - InV_{n1}}$$

This index has been determined at different temperatures for a large number of compounds. Tables are also available.

The value can be used to compare related separations.

Relative retention data

One practical approach for your own data is the use of relative retention.

$$\mathbf{r}_{i,std} = \begin{array}{c} t'_{R(u)} \\ t'_{R(std)} \end{array} = \begin{array}{c} V'_{R(u)} \\ V'_{R(std)} \end{array} = \begin{array}{c} k_{(u)} \\ k_{(std)} \end{array}$$

This is the most common approach. It only requires a single standard.

Relative retention data

To be useful

Standard should be a part of the sample or added to it - internal standard

It should be something that elutes near center of an analysis - although you can use more than one.

Sample size should be small.

Values will remain pretty constant between runs - may vary wildly with a new column.

Retention time, t_R

Simple retention time data is adequate for simple assays like process quality control.

- You already know what is there.
- There are only a few components in the sample (or only a few of interest).

If a true unknown is observed, you can't do much more than note its presence!

Quantitative analysis

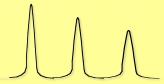
All chromatographic detectors produce a signal that drives a meter, recorder, integrator or A/D converter.

While the detectors used for GC and LC are not the same, quantitation methods are identical.

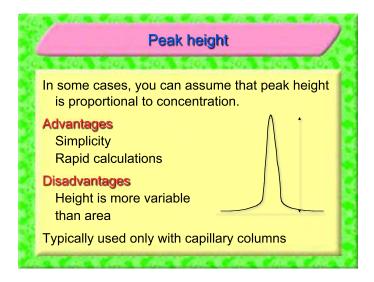
Each detector will produce a response/unit concentration. This is substance dependent so standards must always be used.

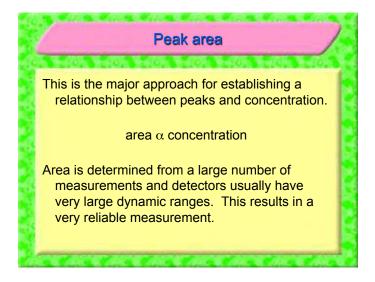
Peaks

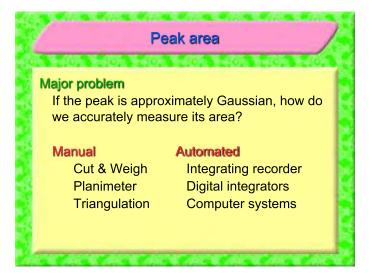
Each method of quantitation assumes that you have one or more reasonably resolved peaks.

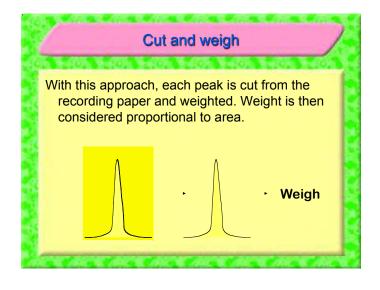


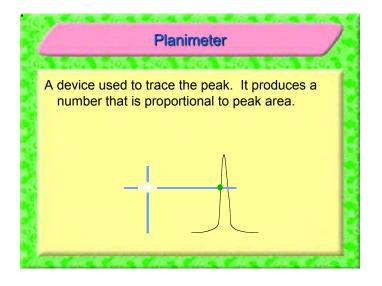
You must be able to find the beginning and end of each peak as well as it's maximum.

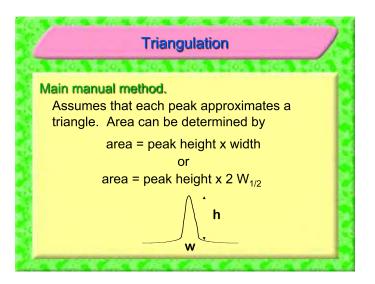


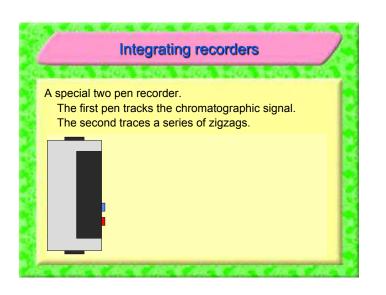












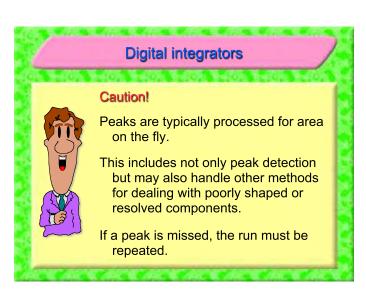
Integrating recorders

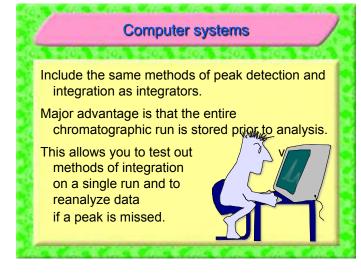
The larger the peak response gets, the more rapidly the second pen sweeps back and forth.

The total number of zigs and zags can then be related to the peak area.

If the peak gets too large, the second pen stops moving. The peak must be kept within the working range.

Rely on A/D conversion of detector response.





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Method	Time, min	Precision, %
Planimeter	15	4.1
Triangulation	10	2.5 - 4
Cut & weigh	20	1.7
Int. Recorder	5	1.3
Integrator	N/A	0.44
Computer	N/A	0.44

Quantitative interpretation

OK, now you have all of your peak areas.

Let's assume you knew what you were doing and all the areas were measured properly.

Big deal!

A relationship between concentration and area must be established or we're just spinning our wheels.

Determining concentration

Several approaches can be used. Use the one that is most appropriate for your method.

Methods we'll cover

External standard method Internal standard method

External standard method

Requirements for proper use:

Standard solution containing all eluents to be quantified.

Standard eluents should be of similar concentration as unknowns.

The standard and sample matrix should be as similar as possible

Analysis conditions must be identical - stable instrument, same sample size ...

External standard method

You either assume that response is linear over the entire concentration range or measure it. Then:

$$conc_{unknown} = \frac{Area_{unknown}}{Area_{known}} conc_{known}$$

This is assuming that the same injection volume was used for both the unknown and standard.

External standard method

Example - determination of X in MeCl₂

Prepare a standard of X

(20.0~mg in $100~ml~MeCl_2)$ - $0.200~\mu g/\mu l$

Use an injection volume of 5 μ l for both the standard and the unknown.

Measure the areas produced by both the sample and the unknown.

Area X_{std} = 2000 units Area X_{unk} = 3830 units

External standard method

Now, determine the concentration of X in you unknown.

$$conc_{unknown} = \frac{Area_{unknown}}{Area_{known}} conc_{known}$$

$$conc_{unknown} = \frac{3830}{2000}$$
 0.200 µg / µl

$$= 0.384 \, \mu g / \mu l$$

You can now convert to a more appropriate concentration if required.

Internal standard method

Overall, the most reliable approach.

Basis

A known substance is added at a constant concentration to all standards and samples - internal standard.

Since the internal standard is always present at a constant amount, it can be used to account for variations such as injection volume during an analysis.

Internal standard method

Requirements for an internal standard.

- Must be present at a constant concentration in all samples and standards.
- Must be stable and measurable under the analysis conditions.
- Must not interfere with the analysis or co-elute with sample components.

Internal standard method

Three common approaches are used

Classical method - weighed portions of the standard and sample are combined

Stock solution - a known volume of the sample is 'spiked' with a known volume of the standard

Calibration plot - a series of standards are run and a curve plotted based on corrected peak areas.

Internal standard method

Regardless of the method for introducing the standard or calibrating, the calculations are the same.

They are the same as with the detector response factor method.

Our NORM substance is now predetermined and a fix value.

Internal standard method

$$C_{ISTD} = f_{ISTD} A_{ISTD}$$
$$C_{unk} = f_{unk} A_{unk}$$

Since the internal standard is assigned a value of 1.00 and is held constant, we can correct for run to run variations by:

$$\mathbf{C}_{\mathsf{unk}} = \begin{array}{cc} \mathsf{A}_{\mathsf{ISTD1}} & \mathsf{A}_{\mathsf{unk}} \\ \mathsf{A}_{\mathsf{ISTD2}} & \mathsf{A}_{\mathsf{known}} \end{array} \quad \mathbf{C}_{\mathsf{known}}$$

known & ISTD1 are obtain from the standard, unk & ISTD2 from the unknown

Internal standard method

It is assumed that variations in the internal standard area are representative of the whole analysis.

Accounts for factors such as:

Sample injection errors or changes Slow detector variations Slow column changes

Internal standard method

Example

Prepare a standard that contains 11.3 mg of X and 12.00 mg of ISTD.

Make several 2 μ l injections and calculate an average response for each component.

Component Average area X 635
ISTD 1009

Internal standard method

Now, inject your unknown.

 $Area_{X} = 990$ $Area_{ISTD} = 1031$

 $C_X = (1009/1031) (990/635) \times 11.3 \text{ mg}$

= 17.24 mg X in the unknown.